

Supercomputing and numerical modelling

Parallel algorithms research lab

VSB TECHNICAL | IT4INNOVATIONS |||| UNIVERSITY | NATIONAL SUPERCOMPUTING OF OSTRAVA | CENTER



Hardware

Ģ	OP 500 The List.	D PRESENTED BY EXAMPLE THE LABORATORY SPECS		OUP d. COUNTRY	FIND OUT MO top500.c CORES	REAT	Power
1	Summit	IBM POWER9 (22C, 3.07GHz), NVIDIA Volta GV100 (80C), Dual-rail Mellanox EDR Infiniband	DOE/SC/ORNL	USA	2,282,544	143.5	11.1
2	Sierra	IBM POWER9 (22C, 3.16Hz), NVIDIA Tesla V100 (80C), Dual-rail Mellanox EDR Infiniband	DOE/NNSA/LLNL	USA	1,572,480	94.6	7.44
3	Sunway TaihuLight	Shenwei SW26010 (260C 1.45 GHz) Custom interconnect	NSCC in Wuxi	China	10,649,600	93.0	15.4
4	Tianhe-2A (Milkyway-2A)	Intel Ivy Bridge (120 2.2 GHz) & TH Express-2, Matrix-2000	NSCC Guangzhou	China	4,981,760	61.4	18.5
5	Piz Daint	Cray XC50, Xeon E5-2690v3 (1202.66Hz), Aries interconnect , NVIDIA Tesla P100	CSCS	Switzerland	319,424	21.2	2.38

PERFORMANCE DEVELOPMENT





1993 1994 1995 1996 1997 1998 1999 2000 2011 2002 2003 2004 2005 2006 2007 2008 2009 2010 2011 2012 2013 2014 2015 2016 2017 2018



ACCELERATORS/CO-PROCESSORS



Next-generation U.S. Department of energy supercomputers



Introduction

A single Apple iPhone 5 has 2.7 times the processing power than the 1985 Cray-2 supercomputer.











Virtual Prototyping



$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u}{\partial x} + \frac{\partial \rho v}{\partial y} + \frac{\partial \rho w}{\partial z} = 0 \tag{1}$$

$$\frac{\partial\rho u}{\partial t} + \frac{\partial(\rho u^2)}{\partial x} + \frac{\partial(\rho uv)}{\partial y} + \frac{\partial(\rho uw)}{\partial z} = -\frac{\partial p}{\partial x} + \nu \left(\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2}\right)$$
(2)

$$\frac{\partial\rho v}{\partial t} + \frac{\partial(\rho uv)}{\partial x} + \frac{\partial(\rho v^2)}{\partial y} + \frac{\partial(\rho vw)}{\partial z} = -\frac{\partial p}{\partial y} + \nu \left(\frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial y^2} + \frac{\partial^2 v}{\partial z^2}\right)$$
(3)

$$\frac{\partial\rho w}{\partial t} + \frac{\partial(\rho uw)}{\partial x} + \frac{\partial(\rho vw)}{\partial y} + \frac{\partial(\rho w^2)}{\partial z} = -\frac{\partial p}{\partial z} + \nu \left(\frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} + \frac{\partial^2 w}{\partial z^2}\right)$$
(4)

$$\frac{\partial\rho E}{\partial t} + \frac{\partial(\rho uE)}{\partial x} + \frac{\partial(\rho vE)}{\partial y} + \frac{\partial(\rho wE)}{\partial z} = -\frac{\partial p u}{\partial x} - \frac{\partial p v}{\partial y} - \frac{\partial p w}{\partial z} + S$$
(5)

Millennium Prize Problem:

https://en.wikipedia.org/wiki/Navier–Stokes_existence_and_smoothness

Parallel Computing

225.3 M Cells, 1351.8 M Unknowns simpleFoam, k-omegaSST

Mesh generated by snappyHexMesh in parallel 2000 time step iter.









- Struna je předepnuta natažena o délku DL
- Ve struně vznikne tzv. předepínací síla T, která je po celé délce konstantní

Známe:

- materiál, ze kterého je struna vyrobena
- zátěž v každém bodě struny (funkce f(x))
- uchycení (tvz. okrajové podmínky)

Hledáme:

• deformaci struny pod zatěžující liniovou silou



PDE

Rovnice rovnováhy v libovolném bodě struny

$$-Tu''(x) = f(x)$$

Eliptická parciální diferenciální rovnice druhého řádu

Poissonova rovnice:

$$rac{\partial^2 u}{\partial x^2} + rac{\partial^2 u}{\partial y^2} + rac{\partial^2 u}{\partial z^2} = f(x,y,z)$$

Laplaceova rovnice:

$$\Delta u=0$$
 ,

Analytické řešení - ("přesné")

- pro jednoduše matematicky popsatelné tvary
- Čtverec
- Kružnice
- Koule
- Válec

. . .

• nebo jejich kombinace v omezené míře

Numerické řešení - ("přibližné")

- Metoda sítí
- Metoda konečných objemů
- Metoda konečných prvků
- Metoda hraničních prvků
- Isogeometrická analýza

X_{n-X} X_{i+1} X_{i-1} **X**_{n-1} \mathbf{v} X; h ∣ h h i-2 X_{i-2} X_{i-1} Xi **X**_{i+1} **X**_{i+2} h h h

x₂

X1

h

h

Rovnice rovnováhy v libovolném bodě struny

$$-Tu''(x) = f(x)$$

Příklad soustavy po diskretizaci struny metodou sítí

$$\begin{pmatrix} 2 & -1 & 0 & \cdots & 0 \\ -1 & 2 & -1 & 0 & & \vdots \\ 0 & -1 & 2 & -1 & \ddots & & \\ & 0 & -1 & \ddots & \ddots & 0 \\ \vdots & & \ddots & \ddots & 2 & -1 \\ 0 & \cdots & 0 & -1 & 2 \end{pmatrix} \begin{pmatrix} u_1 \\ u_2 \\ u_3 \\ \vdots \\ u_{n-2} \\ u_{n-1} \end{pmatrix} = \frac{h^2}{T} \begin{pmatrix} f_1 \\ f_2 \\ f_3 \\ \vdots \\ f_{n-2} \\ f_{n-1} \end{pmatrix} + \begin{pmatrix} u_0 \\ 0 \\ 0 \\ \vdots \\ 0 \\ u_n \end{pmatrix}$$

Ku = f

soustavu řešíme

- přímými řešiči (Gussova eliminace, ...)
- iteračními řešiči (sdružené gradienty, ...)

Second order elliptic partial differential equation

Laplace equation:

 $\Delta u=0$,

Poisson equation :

$$rac{\partial^2 u}{\partial x^2} + rac{\partial^2 u}{\partial y^2} + rac{\partial^2 u}{\partial z^2} = f(x,y,z)$$

Advection diffusion reaction equation

$$rac{\partial c}{\partial t} =
abla \cdot (D
abla c) -
abla \cdot (ec v c) + R$$





Software

- Creating complex model, computational mesh, boundary condition definition, material models preProcesing
- Solution by numerical methods
- Results analysis- postProcessing

Open source: OpenFOAM, Code Saturne, SU², Elmer,... https://www.cfd-online.com/Wiki/Codes#Free_codes

Commercial codes: ANSYS CFD, FLUENT, CFX, StarCCM+,... https://www.cfd-online.com/Wiki/Codes#Commercial_codes

Or try to write it in your own way Matlab,R, Octave, Python, C, C++, Fortran...

Heat Transfer Module Capability List:

Load steps definition for combination of multiple steady-state and time dependent analyses

Transient solvers

- Generalized trapezoidal rule
- Automatic time stepping based on response frequency approach



Nonlinear solvers

- Newton Raphson full and symmetric
- Newton Raphson with constant tangent matrices
- Line search damping
- Sub-steps definition
- Adaptive precision control for iterative solvers

Linear and quadratic finite element discretization

Gluing nonmatching grids by mortar discretization techniques

Full-fledged material models

- nonlinear materials
- isotropic, orthotropic and anisotropic material models
- materials for phase change

Element coordinate system definition – cartesian, polar and spherical

Temperature and time dependent boundary conditions

- linear convection
- nonlinear convection
- heat flow
- heat flux
- diffuse radiation
- heat source
- translation motion



Consistent SUPG and CAU stabilization for Translation Motion (advection), Inconsistent stabilization

Phase Change based on apparent heat capacity method

Boundary element discretization for selected physical applications

Highly parallel multilevel FETI domain decomposition based solver for billions of unknowns for symmetric and nonsymmetric systems with accelerators support and combination of MPI and OpenMP techniques

Asynchronous parallel I/O

Input mesh format from popular open source and commercial packages like OpenFOAM, ELMER or ANSYS

Output to commonly used post-processing formats, VTK and EnSight

Monitoring results on selected regions for statistic and optimization toolchain

Simple text Espreso Configuration File (ecf) for setting all ESPRESO FEM solver parameters without GUI. Control each parameter in ecf file from command line







Parallel solver development

Behaviour of numerically and parallel scalable solvers



Parallel (strong) Scalability

Numerical (weak) Scalability





ESPRESO FEM Highly parallel finite element package for engineering simulations

ESPRESO on TITAN



3rd (9th) in TOP500 LIST

18,688AMD Opteron 6274 16-core CPUs18,688Nvidia Tesla K20X GPUs

2.7 million core hours dedicated to:

- scalability optimization of ESPRESO
- optimization of GPU accelerated version for large scale problems



Weak Scalability Test

Up to **124 billion** DOF on 17576 Compute Nodes (281 216 cores) Heat transfer (Laplace equation)



Problem size [billion DOF] Number of compute nodes [-]

Strong Scalability Test

20 billion DOF on up to 17 576 Compute Nodes (281 216 cores) Heat transfer (Laplace equation)

ORNL Titan 3rd in TOP500 LIST





Latent heat distribution in the wheel



Heat transfer

Response time optimization of the USL sensor - nonlinear transient simulation





Ontinental

Elasticity BVP

$$-\operatorname{div}\boldsymbol{\sigma}^{(k)} = \mathbf{f}^{(k)} \quad \text{in } \Omega^{(k)}$$
$$\sigma_{ij}^{(k)} = c_{ijkl}\varepsilon_{kl}^{(k)} \quad \text{in } \Omega^{(k)}$$
$$\varepsilon^{(k)} = \frac{1}{2} \left(\nabla \mathbf{u} + \nabla^{\top} \mathbf{u} \right) \quad \text{in } \Omega^{(k)}$$
$$\mathbf{u}^{(k)} = \mathbf{0} \quad \text{on } \Gamma_D^{(k)}$$
$$\boldsymbol{\sigma}^{(k)} \mathbf{n}^{(k)} = \mathbf{t}^{(k)} \quad \text{on } \Gamma_N^{(k)}$$

Terms on contact boundary

$$-g(\mathbf{X}) = u_n(\mathbf{X}) - d(\mathbf{X})$$
$$\mathbf{t}_C^m \, \mathrm{d}\gamma_C^m = -\mathbf{t}_C^s \, \mathrm{d}\gamma_C^s$$
$$\mathbf{t}_C^s = t_n \mathbf{n} + t_{1T} \boldsymbol{\tau}_1 + t_{2T} \boldsymbol{\tau}_1$$

Unilateral contact (non-penetration) $u_n - d \le 0, \ t_n \le 0, \ t_n(u_n - d) = 0$

Friction (Tresca or Coulomb) $\|\mathbf{t}_T\|_2 \le F, \begin{cases} \|\mathbf{t}_T\|_2 < F \quad \Rightarrow \ \mathbf{u}_T = \mathbf{0} \\ \|\mathbf{t}_T\|_2 = F \quad \Rightarrow \ \mathbf{u}_T = -c\mathbf{t}_T, \ c \ge 0 \end{cases}$

 $F = \begin{cases} sb & \dots \text{ Tresca} \\ \mathscr{F}|t_n| & \dots \text{ Coulomb} \end{cases}$





Digital Twin Technology

Complex nonlinear multiphysical problem – electric motor

- Electric fields
- Electromagnetism
- Heat transfer
 - heat generated by magnetism
 - cooling system
- Structural Mechanics
 - structural integrity
 - vibration from motion
 - high speed motors
 - influenced by electromagnetism
- Active cooling system
 - fluid flow
- Acoustic
 - generated by fluid flow
 - generated by electromagnetism
 - generated by vibrations





Water pump efficiency optimization





 $\left(\frac{\partial u}{\partial t} + u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y}\right)$ ρ = ---- $\left(\frac{\partial v}{\partial t} + u\frac{\partial v}{\partial x} + v\frac{\partial v}{\partial y}\right)$ =--- $\frac{\partial E}{\partial t} + u \frac{\partial E}{\partial x} + v \frac{\partial E}{\partial y} = \frac{\partial}{\partial x}$ 21 $\partial(up) \ \partial(vp) \ \partial(wr_{-})$





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